

Continue



sulfur dioxide gas.

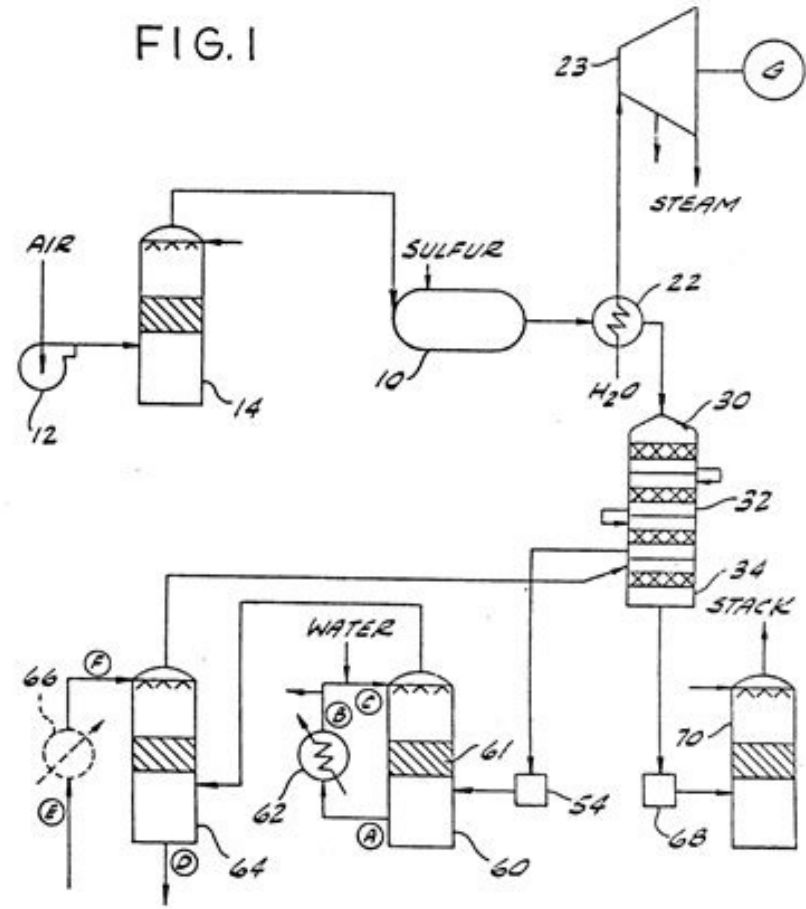
- a. Write a balanced chemical equation for the reaction.
- b. What is the change in the enthalpy (  $\Delta H$  ) of the reaction?
- c. Is this an endothermic or an exothermic reaction?
- d. If 200 grams of sodium sulfite are used in the reaction, how many grams of sodium sulfate will be formed?
- e. If 200 grams of sodium sulfite are used in the reaction, how many kJ of heat will be required for the reaction?

3. Define the terms: endothermic, enthalpy and exothermic.

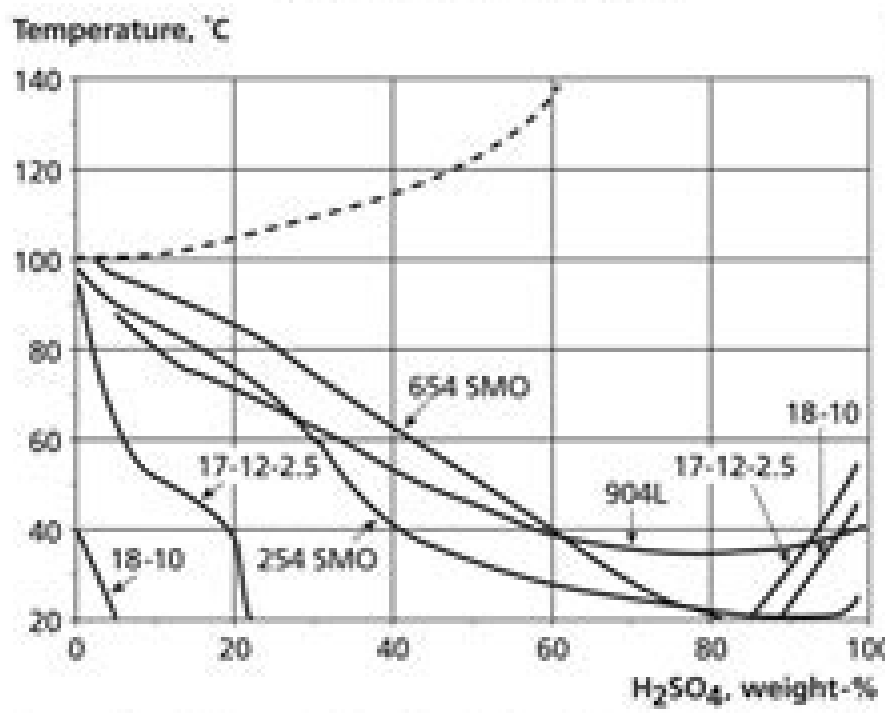
Endothermic:

Enthalpy:

Exothermic:

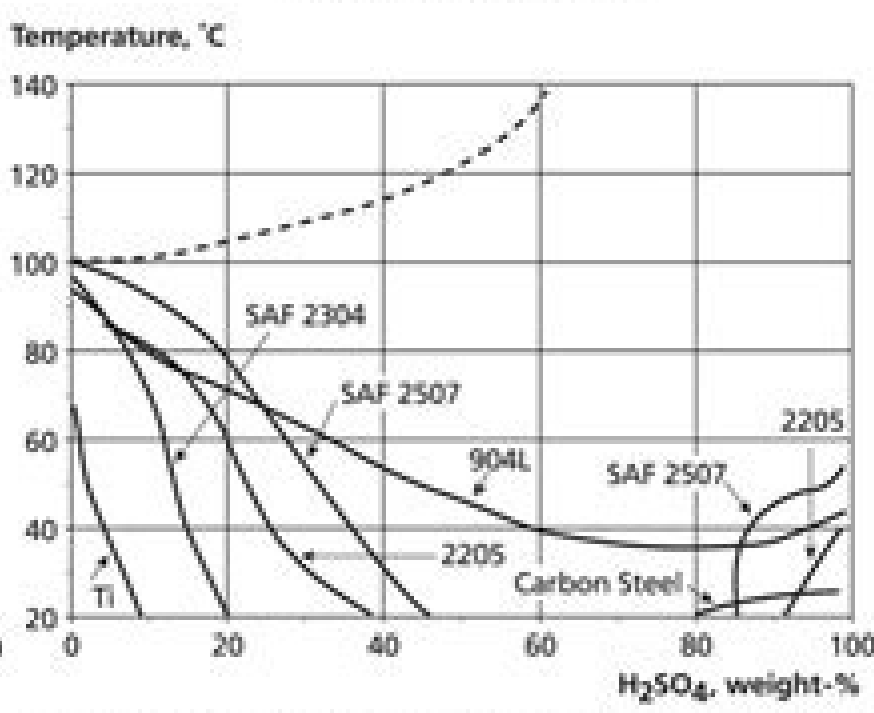


## Pure Sulphuric Acid



Isocorrosion diagram, 0.1 mm/year, for austenitic stainless steels in naturally aerated sulphuric acid of chemical purity. Broken-line curve represents the boiling point.

## Pure Sulphuric Acid



Isocorrosion diagram, 0.1 mm/year, in naturally aerated sulphuric acid of chemical purity. Broken-line curve represents the boiling point.

Specific heat capacity of sulphuric acid. Heat capacity of sulfuric acid solutions.

On fig. Figure 5.1 is a plot of the specific heat  $c_p$  (heat capacity per gram) of aqueous solutions of sulfuric acid at  $T = 298.15$  K as a function of  $A$ , the ratio of moles of water to moles of sulfuric acid. The applied values were taken from very... à [p. 215] Use the heat of solution data in Table B.10 and the heat capacity of the solution to calculate (a) the enthalpy of hydrochloric acid, sulfuric acid or sodium hydroxide of known composition (mole fraction) with respect to pure substance and water at 25 °C (b ) Calculate the heat transfer rate required to or from a process that produces an aqueous solution of HCl, H<sub>2</sub>SO<sub>4</sub>, or NaOH that is diluted or combined with another solution of the same type, and (c) calculate the final temperature at which the aqueous solution formed from HCl, H<sub>2</sub>SO<sub>4</sub> or NaOH, diluted or adiabatically combined with another solution of the same type. Perform material and energy balance calculations for a process involving solutions for which enthalpy versus concentration plots are available. à[S H<sub>2</sub>SO<sub>4</sub> contains two g equivalent). The specific gravity of the solution is 1.230, the heat capacity is 3.00 J/(g·C). Calculate the specific enthalpy of this solution (in kJ/mol H<sub>2</sub>SO<sub>4</sub>) at 60°C relative to pure H<sub>2</sub>O and an infinitely dilute solution at 25°C. à[p.434] Water is added to pure sulfuric acid in a well-insulated room at 25°C and 1 atm to prepare a 4.00 M sulfuric acid solution (DS = 1.231). The final temperature of the product solution must be 25 °C, so the water to be added must be a chilled liquid (T < 25 °C) or a mixture of liquid water and ice. Take one liter of product solution as the basis for calculation and take  $Q_{A//}$  for the process. If you need to know the heat capacity of ice, take half the amount of liquid water. à [p. 435] H<sub>2</sub>SO<sub>4</sub> aqueous,  $r = 49.40$  C) From table 2.217, page 2-185 of Perry's Chemical Engineer's Handbook.Note 1) The heat capacity of a solution of sulfuric acid of the specified composition is 3.85 J/(g·°C).Δ[P.463] A 2.00% molar solution of sulfuric acid is neutralized with a 5.00% molar solution of sodium hydroxide continuously reactor. All reactants enter at 25°C. The standard heat capacity of the sodium sulfate solution is -1.17 kJ/mol Na<sub>2</sub>SO<sub>4</sub>, and the heat capacities of all solutions can be considered as the heat capacities of pure liquid water [4.184 kJ/(kg·C)]. [s.494] The increase in the exothermic reaction temperature depends on three factors: the heat of reaction, the heat capacity of the system, and the heat loss of the system, pre-warmed to 30°C was added all at once to a Dewar flask containing a nitric acid/sulfuric acid solution, also pre-warmed to 30°C. We observed a temperature increase of 17°C in 4 minutes and a decrease of 15°C in the next 4 minutes (Figure 3). Therefore, we estimated the AT to be around 18.5 °C. Since this temperature increase was theoretically scale-independent, we could predict that large-scale nitration reactions would not increase to the temperature of exothermic activity. Based on these results, we felt that this improved nitration process could be safely extended to a pilot plant... à[p. 112] The mechanical stability and ion exchange capacity of these condensation resins were modest. A better approach is to produce a suitable cross-linked basement membrane, which can then be converted to the charged form in a subsequent reaction. Ionics is believed to use this type of diaphragm in many of their systems. In a typical manufacturing process, a mixture of styrene and divinylbenzene is poured onto the intermediate fabricPlates and heated in an oven to form a membrane matrix. The membrane is then sulfonated with 98% sulfuric acid or concentrated sulfur trioxide solution. The degree of swelling of the final membrane is controlled by varying the concentration of divinylbenzene in the initial mixture to control crosslink density. The degree of sulfonation can also vary. The chemistry of this process is .....[401. pp.] A g-mole of pure liquid sulfuric acid mixes with  $r$  g-mole of liquid water at  $T_o$  (°C), also at 7°C (°C), in an adiabatic vessel. The final temperature of the solution is 7.(0). The mass heat capacities of pure acid, pure water, and product solution [J/(g C)] are  $C_{pa}$  and  $C_{ps}$ , respectively, all of which can be assumed to be constant (independent of temperature). [436. S.] Other studies on the heat capacity of sulfuric acid and its aqueous solutions are too numerous to list. However, a recent compendium (9) summarizes most of the work and shows that our assumed heat capacity values for sulfuric acid and its hydrates from room temperature to 80 °C agree with the available literature. 9 0 The reaction flask (volume 500 ml) is equipped with a working stirrer, a reflux condenser and a wide gas inlet tube connecting the end of the condenser to a sulfuric acid sprinkler, an empty safety bottle and a tube running over the surface of the caustic soda. Resorcinol (20 g) and anhydrous ether (150-200 mL) are placed in a reaction flask and anhydrous zinc cyanide (1.5 equivalents) is added. Then a rapid stream of dry hydrogen chloride gas is passed through. The zinc cyanide disappears to form a milky mixture, and as the hydrogen chloride dissolves, the condensation product of the imide hydrochloride separates out as a thick oil that solidifies in 10-30 minutes. The ether is usually saturated in 1.5 hours, after which the hydrogen chloride is slowly removed over an additional 0.5 hour.The ether is then decanted, water (100 ml) is added to the imide hydrochloride, the solution is heated to boiling, filtered and allowed to cool. About half of the aldehyde is separated. After collection, the aldehyde residue crystallizes within 10-15 hours. The total yield is about 95% and its pl. is 135-136° after recrystallization with activated charcoal from water. Changing the pH of the heating solution. In an attempt to determine the optimum pH of the heating solution, tests were carried out with films heated in water adjusted to different pH values with sulfuric acid. In the pH range of 1.1 to 10, both product salinity and flux were proportional to the pH of the heating solution - flux characteristics improve with increasing pH, but at the expense of membrane desalination capacity." [page 130] GRT with particle sizes 1 to 3 mm has been treated using thermal, chemical and combined thermochemical treatments to prepare carbonaceous adsorbents for mercury removal from aqueous solution (Gupta et al., 2011). The adsorbents were prepared by heating the rubber at 400 or 900°C for 2 h under nitrogen and then chemically treating with sulfuric acid, nitric acid or solutions of their mixtures for 24 h. In the thermal treatment of rubber, microporosity, especially mesoporosity, mainly developed. Chemical treatment ensured the formation of macropores. In the case of combined thermochemical treatment, the treatment, which gave the first effect, dominated the effect on the porous structure. The mercury adsorption capacity was greater for adsorbents with higher microporosity [page 753] Gardner, W.L., J.W. Coble, E.K. Jackel, "Thermodynamic Properties of High Temperature Aqueous Solutions. IX. Standard Partial Molar Heat Capacities of Sodium Sulfate and Sulfuric Acid from 0 to 100", J. Phys. Chem., v73, 6, p2017 (1969)... à [p. 474] Preparation of dilute acid can also be dangerous because of the heat generated in the dilution process Concentrated acid is always added to water, not the other way around, to take advantage of the relatively high heat capacity of water. Adding water to concentrated sulfuric acid will cause the sulfuric acid to disperse, or worse, explode. Preparation of solutions above 6 M (35%) is the most hazardous, since the heat generated may be sufficient to bring the dilute acid to a boil, effective mechanical agitation and external cooling (eg, ice bath) are necessary. .144] 5.1. The figure shows a graph of the specific heat  $c_p$  (heat capacity per gram) of aqueous solutions of sulfuric acid at  $T = 298.15$  K as a function of  $A$ , the ratio of moles of water to moles of sulfuric acid. The applied values were obtained from very... [215. p.] Use the heat of solution data in Table B.10 and the heat capacity data of the solution to calculate (a) the enthalpy of a hydrochloric acid, sulfuric acid, or sodium hydroxide solution of known composition (solute mole fraction) with respect to the pure solute and water at 25°C (b) Calculation of the required heat transfer rate to or from a process in which an aqueous solution of HCl, H<sub>2</sub>SO<sub>4</sub> or NaOH is formed, diluted or combined with another solution of the same substance, and c) Calculation of the final temperature if an aqueous solution of HCl, H<sub>2</sub>SO<sub>4</sub> or NaOH diluted adiabatically or mixed with another solution of the same substance. Perform material and energy balance calculations for the process with solutions for which enthalpy-concentration diagrams are available." [358. s.] A solution of sulfuric acid is designated 8H (where B \u003d 1 g-eq / l and 1 mol). H<sub>2</sub>SO<sub>4</sub> contains two g equivalent). The specific gravity of the solution is 1.230, the heat capacity is 3.00 J/(g·C). Calculate the specific enthalpy (kJ/mol H<sub>2</sub>SO<sub>4</sub>) of this solution at 60°C relative to pure H<sub>2</sub>O and an infinitely dilute solution at 25°C [434]. S.] Water is added to pure sulfuric acid.well-insulated flask initially at 25°C and 1 atm to prepare a 4.00 M sulfuric acid solution (DS = 1.231). The final temperature of the product solution should be 25°C, therefore the added water should be chilled liquid (T < 25°C) or a mixture of liquid water and ice. One liter of product solution is taken as the basis for the calculation and  $Q_{A//}$  is taken for the process. If you want to know the heat capacity of ice, consider that it's half liquid water." [435. p.] H<sub>2</sub>SO<sub>4</sub> aq,  $r = 49.40$  C) Z 2.217. Tables, p. 2-185 Perry's Chemical Engineers' Handbook (see footnote 1), the heat capacity of the sulfuric acid solution of the given composition is 3.85 J/(g·°C).463. p.] 2.00 mol% sulfuric acid solution is neutralized with 5.00 mol% sodium hydroxide solution in a continuous reactor. All reagents flow in at 25°C. The standard heat of sodium sulfate solution is -1.17 kJ/mol Na<sub>2</sub>SO<sub>4</sub>, and the heat capacity of all solutions can be assumed as the heat of pure liquid water [4.184 kJ/(kg·C)]. [494. S.] The temperature increase of an exothermic reaction depends on three factors: the heat of reaction, the heat capacity of the system, and the heat loss of the system. Increase of the reaction temperature in the system, without loss of heat, the adiabatic increase in temperature (NT) depends on the heat of reaction and the heat capacity of the system and is independent of scale. To determine the adiabatic temperature rise of this system, a CDMp/sulfuric acid solution preheated to 30°C was added in one portion to a durian flask containing a nitric acid/sulfuric acid solution also preheated to 30°C. We observed a temperature increase of 17 °C in 4 minutes with a temperature decrease of 15 °C in the next 4 minutes (Fig. 3). Therefore, we calculated that AT Since this temperature increase was theoretically scale-independent, we could predict that a large-scale nitration reaction would not increase to the temperature of exothermic activity.As a result, we found this improved nitration method safe for the experimental setup... [112. S.] The mechanical stability and ion exchange capacity of these condensation resins were low. A better approach is to fabricate a suitable cross-linked basement membrane, which can then be converted to the charged form in a subsequent reaction. Ionics are believed to use this type of diaphragm in many of their systems. In a typical manufacturing process, a mixture of styrene and divinylbenzene is poured onto a fabric, pressed between two plates and heated in an oven to form a membrane matrix. The membrane is then sulfonated with 98% sulfuric acid or concentrated sulfur trioxide solution. The degree of swelling of the final membrane is controlled by varying the concentration of divinylbenzene in the initial mixture to control crosslink density. The degree of sulfonation can also vary. The chemistry of this process is .....[401. pp.] A g-mole of pure liquid sulfuric acid mixes with  $r$  g-mole of liquid water at  $T_o$  (°C), also at 7°C (°C), in an adiabatic vessel. The final temperature of the solution is 7.(0). The mass heat capacities of pure acid, pure water, and product solution [J/(g C)] are  $C_{pa}$  and  $C_{ps}$ , respectively, all of which can be assumed to be constant (independent of temperature). [436. S.] Other studies on the heat capacity of sulfuric acid and its aqueous solutions are too numerous to list. However, a recent compendium (9) summarizes most of the work and shows that our assumed heat capacity values for sulfuric acid and its hydrates from room temperature to 80 °C agree with the available literature. 9 0 The reaction flask (volume 500 mL) is equipped with an efficient stirrer, a reflux condenser and a wide gas inlet tube connecting the end of the condenser in series with a nebulizer with sulfuric acid, an empty flask and a passage tube throughsurface of sodium hydroxide solution. Resorcinol (20 g) and anhydrous ether (150-200 ml) were placed in the reaction flask and anhydrous zinc cyanide (1.5 eq) was added. A rapid stream of dry hydrogen chloride gas is then passed through. The zinc cyanide volatilizes to form a milky mixture, and upon dissolution of the hydrogen chloride, the imide hydrochloride condensation product is released as a thick oil that solidifies in 10-30 minutes. The ether is typically saturated within 1.5 hours, then hydrogen chloride is passed through slowly for another 0.5 hours. The ether is then decanted off, water (100 ml) is added to the imide hydrochloride, the solution is heated to boiling, filtered and cooled. About half of the aldehyde is released. The aldehyde residue then crystallizes in 10-15 hours. Total efficiency is about 95%, so pl. is 135-136° after recrystallization from charcoal from water. [Page 943] Changing the pH of the heating solution. In order to determine the optimal pH of the heating solution, tests were carried out on films heated in water brought to different pH values with sulfuric acid. In the pH range from 1.1 to 10, the salt content in the product and the flow were proportional to the pH of the heating solution - the flow characteristics improved with increasing pH, but at the expense of the membrane's demineralization ability. [Pg.130] GRT with particle sizes ranging from 1 to 3 mm has been subjected to thermal, chemical and combined thermochemical treatments to prepare carbon adsorbents to remove mercury from aqueous solution (Gupta et al., 2011). The adsorbents were prepared by heating the rubber to 400 or 900 °C for 2 h in a nitrogen atmosphere, followed by chemical treatment with sulfuric acid, nitric acid or their mixture solutions for 24 h. The heat treatment of the rubber caused mainly microporosity, especially mesoporosity. The chemical treatment ensured the formation of macropores. Internal and chemical treatments, and the treatment that gave the first effect had a dominant effect on the porous structure. The adsorption capacity for mercury is higher for adsorbents with higher microporosity. [Pg.753] Gardner, V.L. JW Cobble, EC Jekel, "Thermodynamic Properties of High-Temperature Aqueous Solutions. IX. Standard Partial Molar Heat Capacities of Sodium Sulfate and Sulfuric Acid from 0 to 100", J. Phys. Chem., v73, 6, p2017 (1969). ....[Pg. 474] Preparation of dilute acid can also be dangerous because of the heat generated in the dilution process Concentrated acid is always added to water, not the other way around, to take advantage of the relatively high heat capacity of water. Adding water to concentrated sulfuric acid will cause the sulfuric acid aerosol to disperse or, worse, explode. 6 M (35%) is the most dangerous, as the heat generated may be sufficient to boil the dilute acid, effective mechanical agitation, and external cooling (e.g., ice bath).

